STOCK BALL JOINTS



Ball joints have been around since the beginning of time. The writer first came across them during World War II where they were used on steam vessels to accommodate pipe expansion and twisting of the hulls. In all probability, they were used exactly the same way in the First World War, as the Liberty Ships of World War II were copies of the same vessels.

All in all, that is about a 100-year history with little difference in design except for the use of better grade materials and improved seals. While thin-walled material like Stainless Steel hoses or the many variations of Stainless Steel expansion joints have very high safety factors, there is comfort in knowing you are using a zero thrust product where no component has a thickness less than the piping itself. One of our overseas reps, in a country where sabotage was common, commented, "They are quite resistant to rifle fire as well."

We were first exposed to the need for ball joints where thermal expansion design centered around the use of high pressure steam for heating. There is one huge steam-generating station in lower New York that continues to supply steam for heating in New York City. Any building owner that purchases this high pressure supply steam must engineer all their high pressure inlet piping to the satisfaction of Con Edison (the steam supplier). The use of ball joints to handle thermal movement is a necessity as space is tight and leaves no room for pipe loops or offsets.



We not only sell our ball joints, but we engineer the systems as well, should there be no specifications or if specifications call for design by vendor.

We look forward to working with you.



BALL JOINT SPECIFICATION

Steel Ball Joints shall have weld ends or fixed and floating flanges. The thrust-free, ball and socket arrangement shall allow 360° of intermittent rotation and a minimum rocking motion of \pm 7.5°. Seals are guaranteed by the high pressure injection of graphite packing in a cavity between reinforced hard graphite and steel rings.

The ball and steel seal retention rings shall be plated with a minimum 1 mil thickness of crack-free hard chrome. The socket must incorporate an adequate number of packing cylinders for uniform distribution of the graphite seal. All cylinders must incorporate a valve to prevent blowback should pumping additional sealing material become necessary while under full line pressure.

Minimum ratings are 250 psi (17 Bar) @ 480°F (250°C).

CERTIFICATIONS MUST INCLUDE:

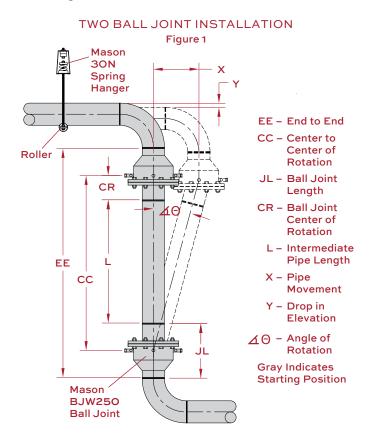
- 1. Either manufacturer's published information or calculations by a P.E. to verify length of spool pieces and the distance between centers of ball joints for the motion with a reasonable safety factor.
- 2. The friction force at the start of motion to be resisted by the anchors.

Should the consulting firm prefer to indicate location of anchors and ball joints as preliminary and leave final selections to job site conditions, the manufacturer must have a P.E. on staff with a minimum of 5 years piping design experience to submit final details to allow motion as well as the force on the anchors to overcome starting friction.

Ball Joints shall be weld end **BJW** or flanged **BJF** as manufactured by Mason Industries, Inc.

TWO BALL JOINTS

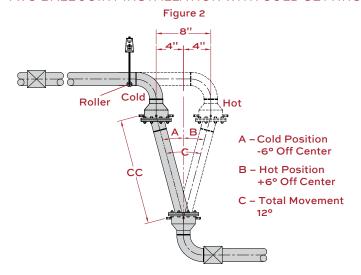
When ball joints are installed at each end of a pipe offset (Fig. 1), the system can accommodate much larger movements with much lower anchorage requirements than solid pipe in the same configuration.



COLD SETTING

One way to increase allowable motion is to start out with the assembly pre-set all the way to the position when the pipe is cold (Figure 2). Assuming the total expansion from Cold (Ambient Temperature) to Hot is 8", you could set the pipe line 4" off center and design for a 4" rather than an 8" movement leg. The piping is preset 6° off center to 6° past center. Maximum rated movement is 7.5° off center, so 6° provides a safety factor.

TWO BALL JOINT INSTALLATION WITH COLD SETTING

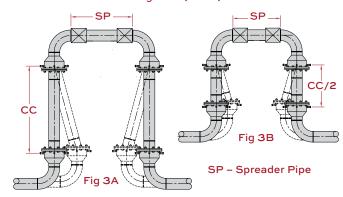


While the method is perfectly valid, steamfitters are accustomed to working "Plumb" and the "Cold Set" instruction can be missed. The method is excellent but supervision becomes essential and the designer must decide whether to take the risk.

FOUR BALL JOINTS

In many cases any offset is undesirable, so four ball joints are used in a loop (Figure 3A). Using the same dimension "CC" in both legs, you can accommodate twice the motion. Reducing the centers 50% would accommodate the same two joint motion (Fig. 1) with smaller offset and conserve space as well (Fig. 3B).

FOUR BALL JOINT INSTALLATION Figure 3 (A & B)



DROP IN ELEVATION "Y"

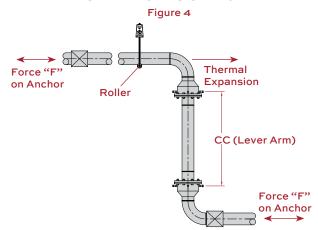
Ball joint movement reduces distance between parallel piping as shown by "Y" (Figure 1). This dimension is significant because if the offset is vertical, the adjacent pipe support could pull out. Therefore a Mason 30N spring hanger with a minimum deflection of 4 times "Y" should be installed at the first support and the second and third locations studied.

STARTING RESISTANCE

Ball joints do not generate any pressure thrust. However, there is an initial force required to start motion that controls anchorage.

The force "F" applied to the pipe anchors is directly related to the distance between Ball Joint Centers "CC" (Figure 4). Force "F" diminishes with longer lever arms needed for larger movements. Four joint loops have shorter levers for the same movement, so forces increase (Table 4).

STARTING RESISTANCE



USING SELECTION TABLES

The following tables provide rounded values for easy selection. For the sake of simplicity, Ball Joint Centers "CC" are in 6" increments in Table 1, and 3" in Table 2. If space is tight, interpolate between columns. Calculations based on Table 5 may save even more space.

The next page provides examples of how to use the tables with the installations previously discussed.



TABLE 1 - "CC", "L", AND "Y" DIMENSIONS FOR TWO JOINT INSTALLATION WITHOUT COLD SETTING (See Figure 1)

Pipe			Pi	ре М	ovem	ent ")	("					
Size	≤4"	5"	6"	7"	8"	9"	10"	11"	12"	CR		
(in)		Ball Joint Centers "CC" (inches)									JL	
2	24	30	36	42	48	54	60	66	72	Center of	Ball Joint	
21/2 - 14	48	60	72	84	96	108	120	132	144	Rotation	Length	
Size		Inte	ermitte	nt Pip	oe Ler	ngth "	L" (inc	hes)		(in)	(in)	
2	16	22	28	34	40	46	52	58	64	4	7	
21/2	40	52	64	76	88	100	112	124	136	41/8	77/8	
3	39	51	63	75	87	99	111	123	135	43/8	81/2	
4	38	50	62	74	86	98	110	122	134	5	101/2	
5	38	50	62	74	86	98	110	122	134	51/8	105/8	
6	37	49	61	73	85	97	109	121	133	55/8	117/8	
8	34	46	58	70	82	94	106	118	130	7	143/8	
10	33	45	57	69	81	93	105	117	129	75/8	16	
12	29	41	53	65	77	89	101	113	125	91/2	18 ¹ /8	
14	27	39	51	63	75	87	99	111	123	101/2	191/4	
Size			Drop ii	n Elev	ation	"Y " (i	nches	()				
2	.34	.42	.50	.59	.67	.76	.84	.92	1.01			
21/2 - 14	(17)	.21	.25	.29	.33	.38	.42	.46	.50			

TABLE 2 - "CC", "L", AND "Y" DIMENSIONS FOR TWO JOINT INSTALLATION WITH COLD SETTING (See Figure 2)

Pipe			ı	Pipe N	/loven	nent "	X"				
Size	≤4"	5"	6"	7"	8"	9"	10"	11"	12"	CR	
(in)	Ball Joint Centers "CC" (inches)									Ball Joint	JL
2	12	15	18	21	24	27	30	33	36	Center of	Ball Joint
21/2 - 14	24	30	36	42	48	54	60	66	72	Rotation	Length
Size		Int	ermitt	ent Pi	pe Le	ngth '	'L" (in	ches)		(in)	(in)
2	4	7	10	13	16	19	22	25	28	4	7
21/2	16	22	28	34	40	46	52	58	64	41/8	77/8
3	15	21	27	33	39	45	51	57	63	43/8	81/2
4	14	20	26	32	38	44	50	56	62	5	101/2
5	14	20	26	32	38	44	50	56	62	51/8	105/8
6	13	19	25	31	37	43	49	55	61	55/8	117/8
8	10	16	22	28	34	40	46	52	58	7	143/8
10	9	15	21	27	33	39	45	51	57	75/8	16
12	5	11	17	23	29	35	41	47	53	91/2	181/8
14	3	9	15	21	27	33	39	45	51	101/2	191/4
Size			Drop	in Ele	vatior	n "Y" (inche	s)			
2	.17	.21	.25	.29	.34	.38	.42	.46	.50		
21/2 - 14	.08	.10	13	.15	.17	.19	.21	.23	.25		

TABLE 3 - MINIMUM SPREADER PIPE "SP" BETWEEN ELBOWS FOR FOUR JOINT INSTALLATION TO AVOID JOINT CLASHING (See Figure 3)

Pipe	Pipe Movement " X"										
Size	≤ 4"	5"	6"	7"	8"	9"	10"	11"	12"		
(in)	Sp	Spreader Pipe "SP" between Elbows (inches)									
2	18	21	24	27	30	30	30	33	36		
21/2	18	21	24	27	30	30	30	33	36		
3	18	21	24	27	30	30	30	33	36		
4	24	24	24	27	30	30	30	33	36		
5	24	24	24	27	30	30	30	33	36		
6	18	21	24	27	30	30	30	33	36		
8	18	21	24)	27	30	30	30	33	36		
10	18	21	24	27	24	27	30	33	36		
12	18	21	24	27	24	27	30	33	36		
14	12	15	18	21	24	24	24	27	30		



TABLE 4 - STARTING RESISTANCE AT 250 PSI (See Figure 4)

Pipe	Torque	Pipe Movement "X"										
Size	"T"	≤ 4"	≤ 4"	6"	6"	8"	8"	10"	10"	12"	12"	
(in)	(ft-lb)	F	orce "F	" (lb) o	n Anch	ors Wi	thout 8	Cold S	Setting			
2	200	200	400	133	267	100	200	80	160	67	133	
21/2	230	115	230	77	153	58	115	46	92	38	77	
3	320	160	320	107	213	80	160	64	128	53	107	
4	600	300	600	200	400	150	300	120	240	100	200	
5	1000	500	1000	333	667	250	500	200	400	167	333	
6	2000	1000	2000	667	1333	500	1000	400	800	333	667	
8	3300	1650	3300	1100	2200	825	1650	660	1320	550	1100	
10	6000	3000	6000	2000	4000	1500	3000	1200	2400	1000	2000	
12	7500	3750	7500	2500	5000	1875	3750	1500	3000	1250	2500	
14	11000	5500	11000	3667	7333	2750	5500	2200	4400	1833	3667	

TABLE 5 - BALL JOINT ANGULAR MOVEMENT

Pipe Size (in)	Maximum Angle	O Recommended Angle with 20% Safety Factor
2	30°	24°
21/2 - 14	15°	12°

In all engineered systems, a safety factor is important.

TWO BALL JOINT INSTALLATION WITHOUT COLD SETTING

To size an 8" two ball joint offset for 6" movement at 250 psi, use Table 1. The recommended Center to Center "CC" is 72" the Intermediate Pipe Length "L" is 58" and the Drop in Elevation "Y" is 0.25". Table 4 shows the Force "F" on Anchor as 1100 lb. A stainless expansion joint thrust is 12,000 lb, 11 times the required anchorage for the ball joints.

TWO BALL JOINT INSTALLATION WITH COLD SETTING

To size an 8" two ball joint offset for 6" movement at 250 psi with cold set, use Table 2. The recommended Center to Center "CC" is 36" the Intermediate Pipe Length "L" is 22" and the Drop in Elevation "Y" is 0.13") Table 4 shows the Force "F" on Anchor as 2200 lb This force is still much lower than the stainless expansion joint thrust of 12,000 lb, which is 5.5 times the required anchorage for the ball joints.

FOUR BALL JOINT INSTALLATION WITHOUT COLD SETTING

To size an 8" four ball joint loop for 6" movement, divide the 6" movement by two, as there are two 3" movement legs. Using Table 1, 4" column, "CC" is 48" "L" is 34" and "Y" is 0.17" To size the spreader pipe "SP" so the two legs of the loop do not clash, use Table 3 for a Minimum Spreader Length "SP" of 24"

"Cold Set" designs are the same as above, using Table 2.

FRICTION FORCES

Pipe Friction is usually taken as 30% of the pipe weight between anchors. Add this force to Table 4 or calculated numbers as an additional force on anchors.

CALCULATIONS

For engineers who prefer to do their own calculations. Refer to Figure 1 for definitions of "CC", "L", "CR", "EE", "JL" and "Y"; Table 4 for "F" and "T"; and Table 5 for " Θ ".

TWO BALL JOINT INSTALLATION WITHOUT COLD SETTING

Example: 10" steam line, thermal expansion 7".

 $CC = X / [Sin (\Theta/2)] = 7" / [Sin (12°/2)] = 67"$

 $L = CC - (2 \times CR) = 67'' - (2 \times 7.625'') = 51.75''$

 $EE = L + (2 \times JL) = 51.75" + (2 \times 16") = 83.75"$

 $Y = CC - (CC^2 - X^2)^{1/2} = 67'' - (67^2 - 7^2)^{1/2} = 0.37''$

For 0.37" movement, we recommend a spring hanger with a deflection 4 times "Y" or 1.48", i.e. Mason 1.5" deflection 30N hanger.

F = 2T / CC = 2 x 6000 ft-lb / 5.58 ft = 2151 lb

TWO BALL JOINT INSTALLATION WITH COLD SETTING

Example: 10" steam line, thermal expansion 9".

 $CC = [X/2] / [Sin(\Theta/2)] = [9"/2] / [Sin (12°/2)] = 43"$

L = CC - (2 x CR) = 43" - (2 x 7.625") = 27.75"

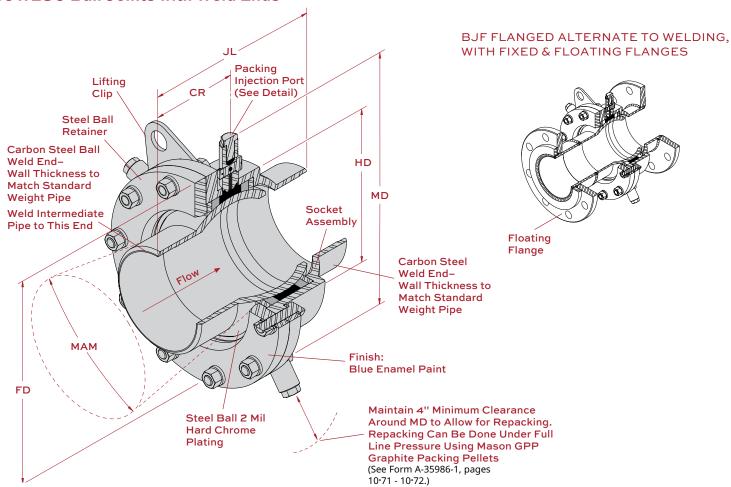
EE = L + (2 x JL) = 27.75" + (2 x 16") = 59.75"

 $Y = CC - (CC^2 - (X/2)^2)^{1/2} = 43'' - (43^2 - (9/2)^2)^{1/2} = 0.24''$

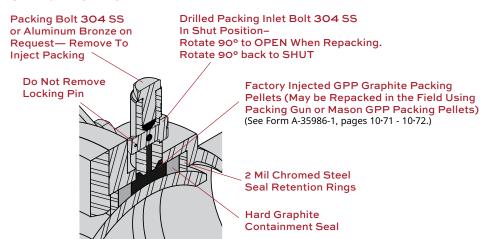
For 0.24" movement, we recommend a spring hanger with a deflection 4 times "Y" or 0.96", i.e. Mason 1" deflection 30N hanger.

 $F = 2T / CC = 2 \times 6000 \text{ ft-lb} / 3.58 \text{ ft} = 3352 \text{ lb}$

BJW250 Ball Joints with Weld Ends



SEAL & PACKING DETAIL



TYPE BJW250 DIMENSIONS & PRESSURE RATINGS

Туре	Pipe Size (in)	JL Joint Length (in)	CR Center of Rotation (in)	FD Flange Diameter (in)	HD Hub Diameter (in)	MD Max. Diameter (in)	MAM Max. Angular Movement (degrees)	Maximum Pressure @ 480°F (psi)	Starting Resistance Torque (ft/lb)	Number of Ports	Ship Weight (lb)
	2	71/2	4	_	51/4	115/8	30	250	200	2	16
	21/2	77/8	41/8	_	57/8	123/8	15	250	230	2	23
	3	81/2	41/4	_	65/8	13	15	250	320	2	26
	4	105/8	51/4	107/8	77/8	141/4	15	250	600	4	72
BIW250-	5	105/8	51/8	12	9	151/2	15	250	1000	4	80
БЈVV250-	6	113/4	53/4	131/4	101/2	163/4	15	250	2000	5	113
	8	141/4	67/8	16	127/8	191/4	15	250	3300	6	189
	10	16	73/4	193/8	16	215/8	15	250	6000	7	280
	12	181/4	93/8	217/8	183/8	241/2	15	250	7500	8	361
	14	193/4	91/2	241/2	201/8	257/8	15	250	11000	9	443

